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**(56) Documents Cited**

**EP 0105828 A2      US 5094218 A      US 4333440 A**  
**US 4185604 A**

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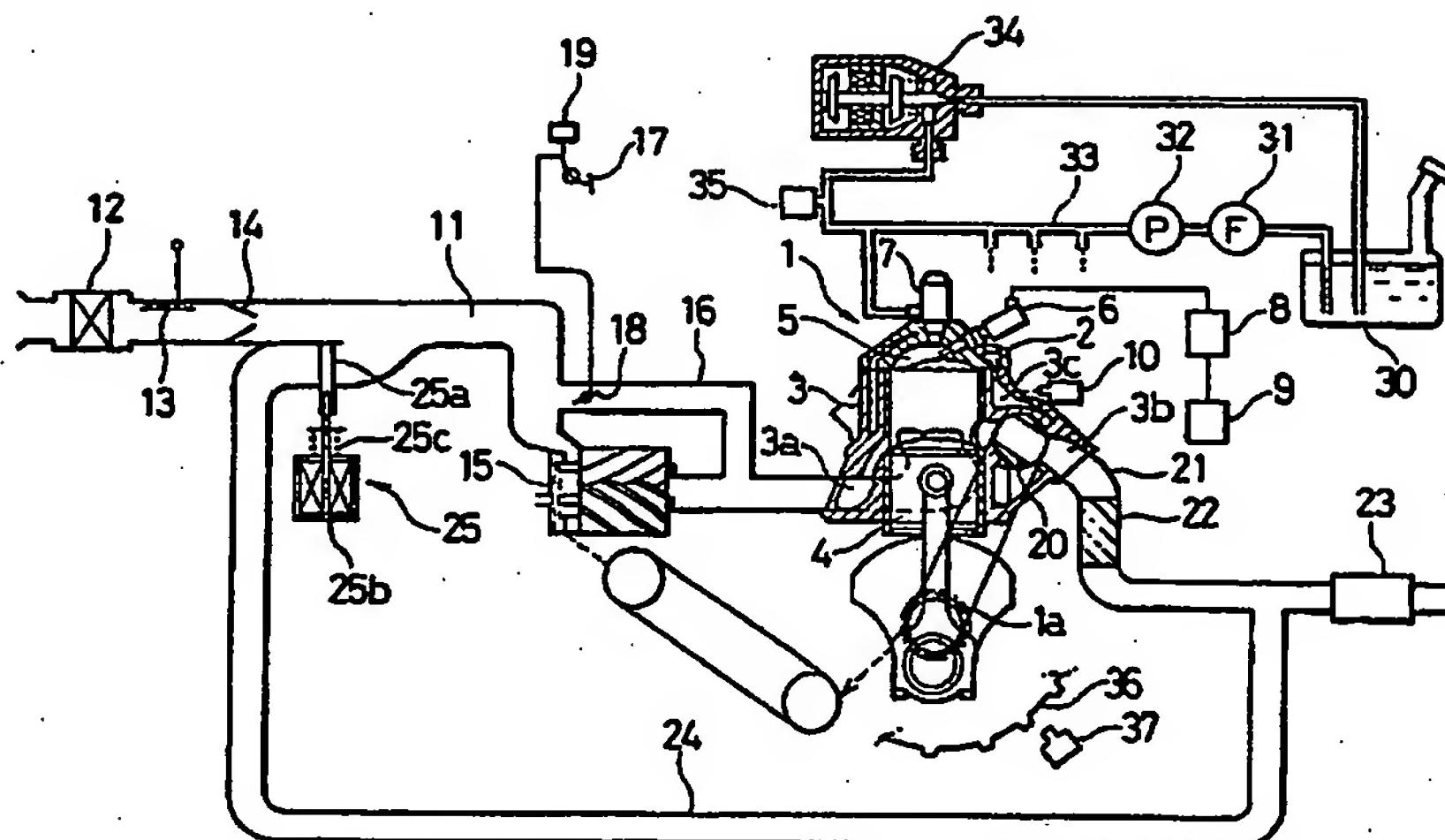
(72) Inventor(s)

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**(54) I.c.engine exhaust gas recirculation control**

(57) The current supplied to the solenoid 25b or a stepping motor operating the exhaust recirculation slide valve 25a is determined from a map or formula depending on accelerator pedal position or intake air quantity and the engine coolant temperature and speed. The valve opening is proportional to the current.

**FIG.1**



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FIG.1

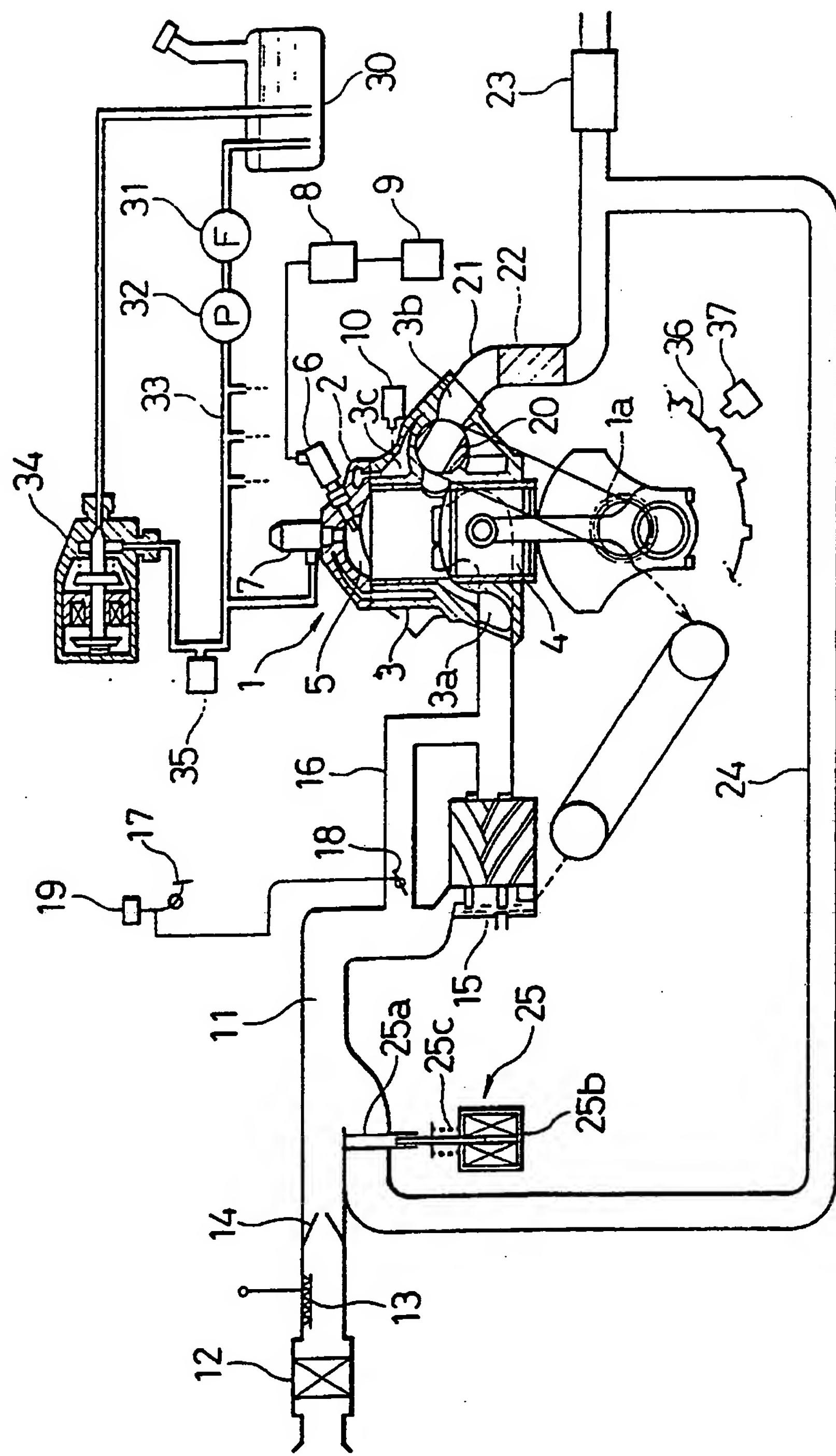
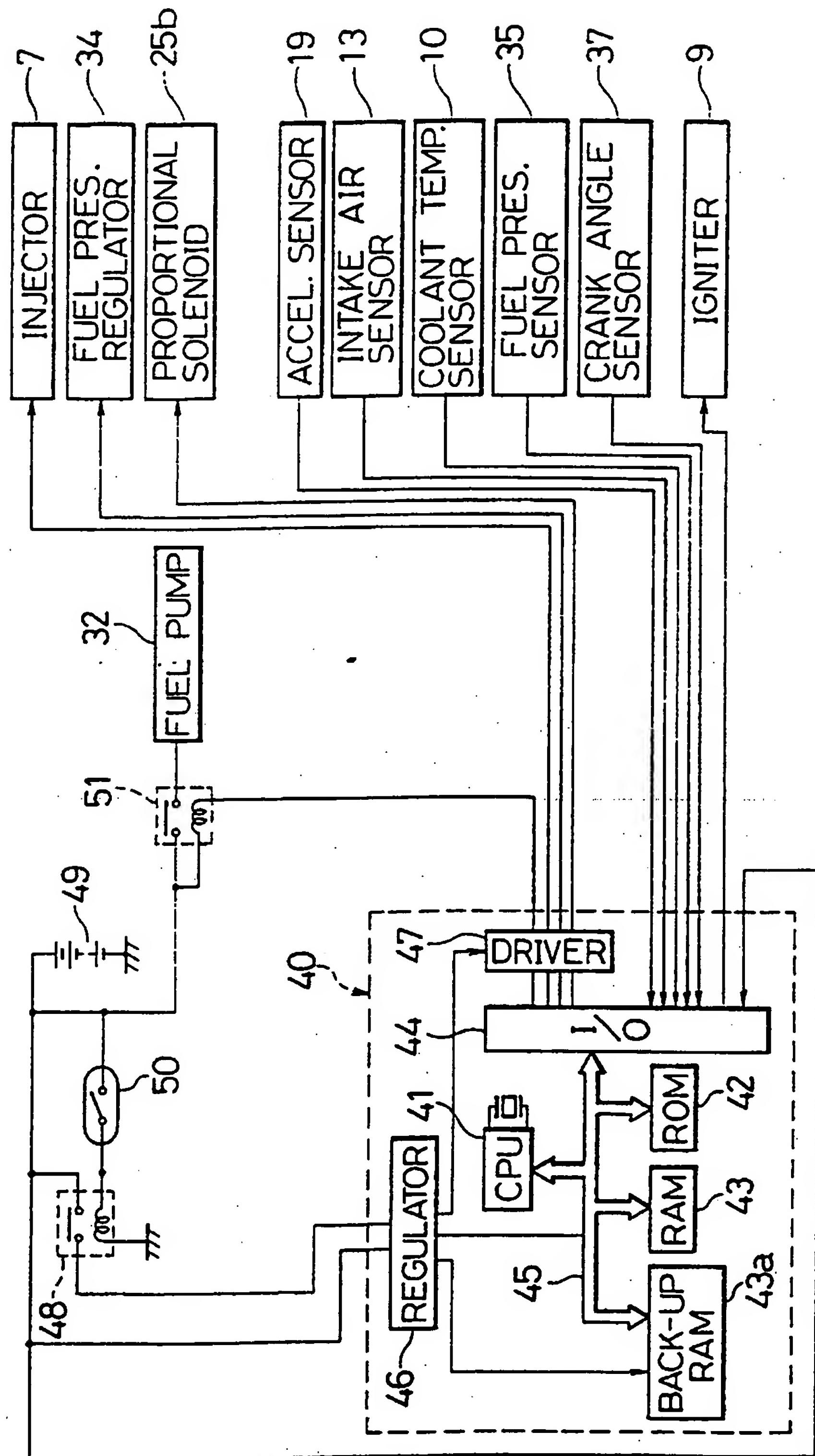


FIG.2



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FIG.3

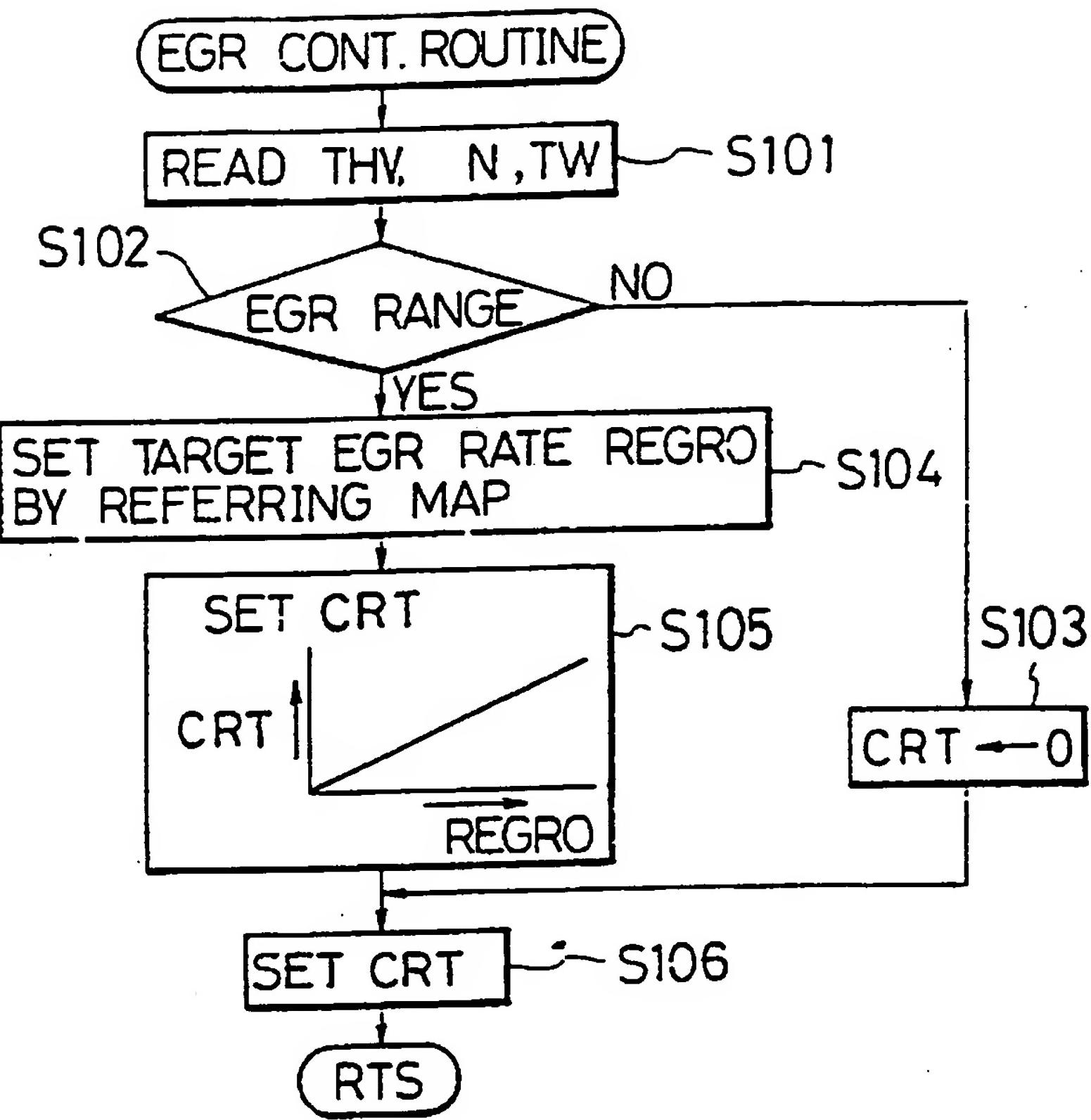


FIG. 4

DESCRIPTIONEXHAUST GAS RECIRCULATION CONTROL METHOD

The present invention relates to a method for controlling the amount of exhaust gases recirculated into an induction air conduit and more specifically, but not exclusively, to a method for an engine needing a relatively high recirculation rate of exhaust gas.

This application is divided out of application 9316919.1, which relates to a method and apparatus for recirculating exhaust gas.

As is well known, there are many engines being equipped with an exhaust gas recirculation (hereafter referred to as "EGR") system in recent years. The EGR system is one of exhaust emission control systems by which NO<sub>x</sub> emission is reduced through recirculating a part of the exhaust gas into an induction system and reducing the combustion temperature.

Commonly in the conventional EGR system, a take-out port for exhaust gas is disposed in the vicinity of an exhaust port of an engine and the exhaust gas is returned to an induction system of an engine through a control valve.

On the other hand, as disclosed in Japanese patent application laid open No. 1988-78256, it is proposed that in an EGR system in which a plurality of

exhaust manifolds are provided and a catalytic converter is disclosed corresponding to each exhaust manifold, take-out port of exhaust gas is located at the downstream portion of the catalytic converter.

In a conventional engine where an air-fuel ratio control is carried out near the theoretical air-fuel ratio, an EGR rate (a rate of exhaust gas against induction air) has an upper limit near at most 20% because of a problem of combustion stability, although generally it is not necessary to recirculate as much exhaust gas.

However, in two cycle engine, especially a two cycle engine having a high pressure direct injection system (injecting fuel into a cylinder with high pressure) or a four cycle lean burn engine, a present 3-way catalyst which reduces CO, HC and NOx simultaneously at the theoretical air-fuel ratio is not effective. Therefore, an EGR is inevitably necessary to reduce NOx emission. In this case a very high EGR rate, for example 40% to 50% of the EGR rate is needed. Namely, a large amount of recirculation gas is needed to reduce NOx emission.

Also, the lower the temperature of the recirculated exhaust gas is, the more the combustion temperature goes down, and thereby the formation of NOx is suppressed.

Furthermore, since a two cycle engine with a high pressure direct injection system or a four cycle lean burn engine have a relatively high oxygen concentration in the exhaust gas, it is necessary to let flow exhaust gas more than several times as much as in the case of a conventional engine, and consequently the conventional EGR system comes substantially short of a flow capability in the recirculated exhaust gas.

In view of the foregoing, it is an object of the invention to provide an EGR system which can introduce a large quantity of recirculation gas into an engine needing a large amount of EGR gas, whereby it is able to reduce NOx emission therefrom substantially.

It is another object of the invention to provide an EGR system which can reduce NOx emission more efficiently by introducing a large amount of low temperature recirculation gas into the induction system.

In accordance with a first aspect (not forming part of the present invention), there is provided an exhaust gas recirculation (EGR) system having an EGR control valve for reducing the NOx emission in an internal combustion engine by recirculating a portion of exhaust gases into an induction air conduit through an EGR passageway, the system comprising:-

A take-out port for exhaust gases, located at a portion of an exhaust pipe downstream of a catalytic converter and upstream of a muffler; and

an electrically operative EGR control valve disposed at a confluence portion of said induction air conduit and said EGR passageway so as to control the amount of the recirculated exhaust gas in accordance with the opening area of said EGR control valve.

In accordance with a second aspect (not forming part of the present invention), there is provided a method for connecting an exhaust pipe and an induction air conduit through an EGR passageway, the method comprising the steps of:

disposing a take-out port of exhaust gases at a portion of said exhaust pipe downstream of a catalytic converter and upstream of a muffler; and

disposing an introduction port of exhaust gases into said induction air conduit at a portion of said induction air conduit downstream of an air cleaner and upstream of a by-pass control valve of a two cycle engine or a throttle valve of a four cycle engine.

In accordance with a third aspect, in accordance with the present invention, there is provided a method for controlling the amount of exhaust gases recirculated into an induction air conduit, the method comprising the steps of:

detecting a coolant temperature, an engine speed  
and a throttle opening;

obtaining a target EGR rate by referring to a  
predetermined map; and

determining a value of electrical current applied  
to a proportional solenoid of an EGR control valve.

Disclosed herein is an EGR system of an internal  
combustion engine such as two cycle direct fuel  
injection engine and four cycle lean burn engine in  
which a 3-way catalyst system is ineffective for  
reducing NO<sub>x</sub> emission.

The method herein includes providing a take-out  
port for the recirculation gas downstream of a  
catalytic converter and upstream of a muffler so as to  
supply a low temperature exhaust gas.

The apparatus includes a recirculation gas  
control valve located at a confluence portion of the  
induction air and the recirculation gas for  
controlling the amount of recirculation gas in  
proportion to the opening area of the recirculation  
gas control valve.

By way of example only, a specific embodiment of  
the present invention will now be described, with  
reference to the accompanying drawings, in which:-

Fig. 1 is a schematic diagram showing the engine  
control system;

Fig. 2 is a diagrammatic view of the electronic control system;

Fig. 3 is a flowchart indicating the EGR control routine;

Fig. 4 is a schematic view of the map for determining the opening degree of the recirculation gas control valve.

Referring to Fig. 1, reference numeral 1 denotes an engine. In this reference, the engine illustrates a two cycle four cylinder engine. A cylinder block 3 and a piston 4 form a combustion chamber 5 wherein a spark plug 6 and a fuel injector 7 are disposed. The spark plug 6 is connected to the secondary side of an ignition coil 8 and an igniter 9 is connected with the primary side of the ignition coil 8.

Further, a scavenging port 3a and an exhaust port 3b are provided in the cylinder block 3 and in a coolant passageway 3c of the cylinder block 3 a coolant temperature sensor 10 is disposed. Also, an air delivery pipe 11 (corresponding to an air intake pipe of a four cycle engine) is connected to the above scavenging port 3a. Along the air delivery pipe 11 there are provided an air cleaner 12, an air flow sensor (in this embodiment an air flow sensor of a hot wire type) 13, a check valve 14 and a scavenging pump 15 which is driven by a crank shaft 1a in order from

upstream to downstream. The scavenging pump 15 acts to supercharge induction air and scavenge the combustion chamber forcedly.

In a by-pass passage 16 by-passing the above scavenging pump 15 a by-pass control valve 18 operatively linked with an accelerator pedal is provided. An accelerator pedal opening sensor 19 is coupled with the accelerator pedal. In the abovementioned exhaust port 3b, an exhaust rotary valve 20 which is mechanically interlocked with the crankshaft 1a is disposed. An exhaust pipe 21 is coupled with the exhaust port 3b through this rotary valve 20. In the exhaust pipe 21, a catalytic converter 22 for processing CO and HC and a muffler 23 are installed. An EGR passageway 24 extends from a portion between the catalytic converter 22 and the muffler 23. In this reference the catalytic converter is composed of a metal type catalyst.

The EGR passageway 24 is led to an EGR control valve 25 installed at the downstream portion of the check valve 14 in the air delivery pipe 11. The EGR control valve 25 serves for preventing a back-flow of the exhaust gas together with the delivery air. The abovementioned EGR passageway 24 has a large enough cross-sectional conduit area to secure a sufficient gas flow.

The EGR control valve 25 is composed of a plate-shaped slide valve 25a and a proportional solenoid 25b for varying the opening of the slide valve 25a. The slide valve 25a is always forced to be on the closing side by the force of a spring 25c. The above proportional solenoid 25b is driven by the electric current from an ECU 40 which will be described hereafter. The position of the slide valve 25a varies according to the electric current.

On the other hand, a numeral 30 denotes fuel tank from which a fuel filter 31, a fuel pump 32 and a fuel supply conduit 33 are disposed in this order and the fuel supply conduit 33 is connected to a fuel injector 7 of each cylinder. The fuel supply pressure is regulated by a fuel pressure regulator 34 being connected with the fuel supply conduit 33. At the inlet side of the above fuel pressure regulator 34, a fuel pressure sensor 35 is arranged. When a fuel pressure signal detected by the fuel pressure sensor 35 is input to the ECU 40, a drive current output from this ECU 40 to the above fuel pressure regulator is feedback-controlled and thus return fuel is controlled by the change of the valve opening of the fuel pressure regulator 34. As a result, the fuel pressure is controlled at a desired value.

Furthermore, a crank rotor 36 is coaxially

coupled with the crankshaft 1a. At the outer periphery of the crank rotor 36, a crank angle sensor 37 in the form of an electromagnetic pick-up or other type is disposed.

The sensors and actuators described before are controlled by the ECU 40 as shown in Fig. 2. The ECU 40 is composed of a CPU 41, a ROM 42, RAM 43, a backup RAM 43a, an I/O interface 44, a bus line 45, a regulator 46 for supplying a stable specified electric power source to miscellaneous electronic devices and a driver 47 for driving an injector 7, fuel pressure regulator 34 and a proportional solenoid 25b.

The above regulator 46 is connected with a battery 49 through a relay contact of an ignition relay 48 and at the same time it is connected directly with the battery. When an ignition key switch 50 connecting a relay coil of the ignition relay 48 and the battery 49 is turned on and also a relay contact of the ignition relay 48 is closed, the electrical power is supplied to devices. However, even when the ignition key switch is turned off, the electrical power continues to be supplied to the backup RAM 43a. Further, the battery 49 is connected with a relay coil of the fuel pump relay 51 and the fuel pump 32 through a relay contact of the fuel pump relay 51.

An input port of the I/O interface 44 is

connected with an air flow sensor 13, an accelerator pedal opening sensor 19, a coolant sensor 10, a fuel pressure sensor 35 and a crank angle sensor 37. Also this input port is connected to the battery 49 so as to monitor the battery voltage.

On the other hand, an output port of the above I/O interface 44 is connected to an igniter 9 and further through a driver 47 to a fuel injector 7, a fuel pressure regulator 34, a relay coil of a fuel pump relay 51 and a proportional solenoid 25b of an EGR control valve 25.

The ROM 42 aforementioned stores a control programme and miscellaneous fixed control data and the RAM 43 stores the data processed based on the signals from the above sensors and switches and further the data processed by the above CPU 41. Electric power is always supplied to the above backup RAM 43a so as to hold such data as trouble codes for self-diagnosis even after an ignition key switch is turned off. In the above CPU 41 the fuel injection amount and the ignition timing are determined according to the control programme memorised in the ROM 42 and also when an engine is at a condition needing EGR, a value of electric current output to the solenoid 25b of the EGR control valve 25 is determined. According to the electric current above mentioned an opening area of

the EGR control valve 25, namely, an amount of EGR is determined.

Next, an operation of the EGR control valve by the above ECU 40 is described according to a flowchart in Fig. 3. Fig. 3 indicates an EGR control routine which is carried out at a specified time interval.

First, at a step S101 an accelerator pedal opening  $T_{HV}$  in the accelerator pedal opening sensor 19, an engine speed N based on a signal from the crank angle sensor 37 and a coolant temperature  $T_W$  in the coolant temperature sensor 10 are read. Next, the process goes to a step S102 where it is judged whether or not an accelerator pedal opening  $T_{HV}$  and a coolant temperature  $T_W$  are satisfied with a specified condition respectively to see whether or not an engine is in the condition needing EGR. Further at the step S102, if it is judged that an engine is not in the condition needing EGR, the process is diverted from the step S102 to a step S103 where a value of electric current (hereafter referred to as "CRT") is set to 0 ( $CRT = 0$ ) and the process goes to a step S106. At the step S106, the CRT which has been established at the step S103 is set to the signal to be output to the driver 47 from the I/O port 44 and the routine returns to the main routine. That is to say, in case where an engine is not in the condition needing EGR, the

proportional solenoid 25b is rendered off by the zero current, whereby an EGR passage 24 is shut off by the slide valve 25a.

On the other hand, at the step S102, if it is judged that an engine is in the condition needing EGR, the process goes from the step S102 to a step S104 where a target EGR rate  $R_{EGRO}$  (%) is determined by referring to a target EGR rate map stored in the ROM 42 with an interpolative calculation based on an acceleration pedal opening  $T_{HV}$  and an engine speed N. In the abovementioned target EGR rate map optimum values of the EGR rate obtained experimentally are stored as target values as shown in Fig. 4. In this embodiment an accelerator pedal opening  $T_{HV}$  is employed as a parameter indicating an engine load, however it is not necessary to limit to the  $T_{HV}$  value. For example, an induction air amount Q may be used alternatively.

At the next step S105, an electric current CRT to be applied to the proportional solenoid 25b is determined based on an EGR rate  $R_{EGRO}$  set at the step S104. Since the CRT corresponds to an opening of the slide valve 25a and the opening thereof is proportional to an EGR amount, a relationship between  $R_{EGRO}$  and CRT is expressed in a linear function as shown in the step S105. Therefore, the CRT can be

obtained either by a reference to a map or a calculation using a formula.

Then, the process goes from the step S105 to a step S106 where the CRT determined above is set so as to be output to the driver 47 from the I/O port 44 and the routine returns to the main routine. When the electric current CRT is applied to the proportional solenoid 25b of the EGR control valve 25, the slide valve 25a is moved to a position corresponding to the electric current CRT against the spring 25c force, thus the EGR valve opening is maintained such that the EGR amount becomes a target EGR rate REGRO

Because the EGR passage has a sufficient cross-sectional conduit area to obtain of a sufficient amount of the EGR gas and besides a take-out port of the EGR gas is located upstream of the muffler 23 and downstream of the exhaust pipe 21, it becomes possible to supply a large amount of the cold (high density) recirculation gas to the engine. Also there is another advantage that adverse effects of the back pressure on the gas exchange in a cylinder can be minimised. It is further possible that the NOx emission is reduced more efficiently than a conventional EGR system by lowering the cylinder gas temperature before combustion in a four cycle lean burn engine using the present EGR system as well as a

two cycle engine as shown in this example.

The EGR control valve 25 in this embodiment is composed of a slide valve 25a and a solenoid 25b but other constructions using a stepping motor or a similar device instead of a solenoid 25a may be considered.

In summary, disclosed herein is an EGR control system in which:-

a take-out port of the EGR gas is disposed upstream of the muffler and downstream of the exhaust pipe and an EGR control valve by which the recirculation gas amount is controlled is installed at the junction of the recirculation gas and the induction air, whereby it becomes possible to supply a large quantity of the recirculation gas to an engine. When the EGR system according to the present invention is applied to a two cycle engine or a four cycle lean-burn engine, an excellent effect is obtained in reducing NO<sub>x</sub> emission or fuel consumption.

While the presently preferred embodiment of the present invention has been shown and described, it is to be understood that this disclosure is for the purpose of illustration and that various changes and modifications may be made without departing from the scope of the invention as set forth in the appended claims.

CLAIMS

1. A method for controlling the amount of exhaust gases recirculated into an induction air conduit, the method comprising the steps of:
    - detecting a coolant temperature, an engine speed and a throttle opening;
    - obtaining a target EGR rate by referring to a predetermined map; and
    - determining a value of electrical current applied to a proportional solenoid of an EGR control valve.
  2. A method for controlling the amount of exhaust gases recirculated into an induction air conduit, substantially as herein described, with reference to an as illustrated in, the accompanying drawings.
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**Patents Act 1977**  
**Examiner's report to the Comptroller under Section 17**  
**(The Search report)**

Application number  
**GB 9513119.9**

**Relevant Technical Fields**

- (i) UK Cl (Ed.N) F1B  
(ii) Int Cl (Ed.6) F02D 21/08; F02M 25/07

Search Examiner  
**R J DENNIS**

Date of completion of Search  
**26 JULY 1995**

**Databases (see below)**

(i) UK Patent Office collections of GB, EP, WO and US patent specifications.

Documents considered relevant following a search in respect of Claims :-  
**1 AND 2**

(ii)

**Categories of documents**

- |    |   |    |   |
|----|---|----|---|
| X: | Document indicating lack of novelty or of inventive step.   | P: | Document published on or after the declared priority date but before the filing date of the present application.        |
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Category	Identity of document and relevant passages			Relevant to claim(s)
Y	EP 0105828 A2	(AMBAC)		1
Y	US 5094218	(SIEMENS)		1
Y	US 4333440	(BOSCH)		1
X	US 4185604	(NISSAN)		1

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